

# INSIDE Metal Additive Manufacturing

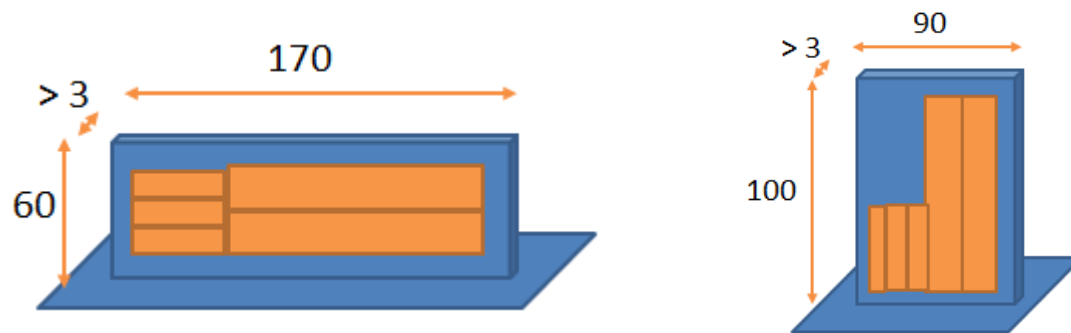
## LMD processing and testing

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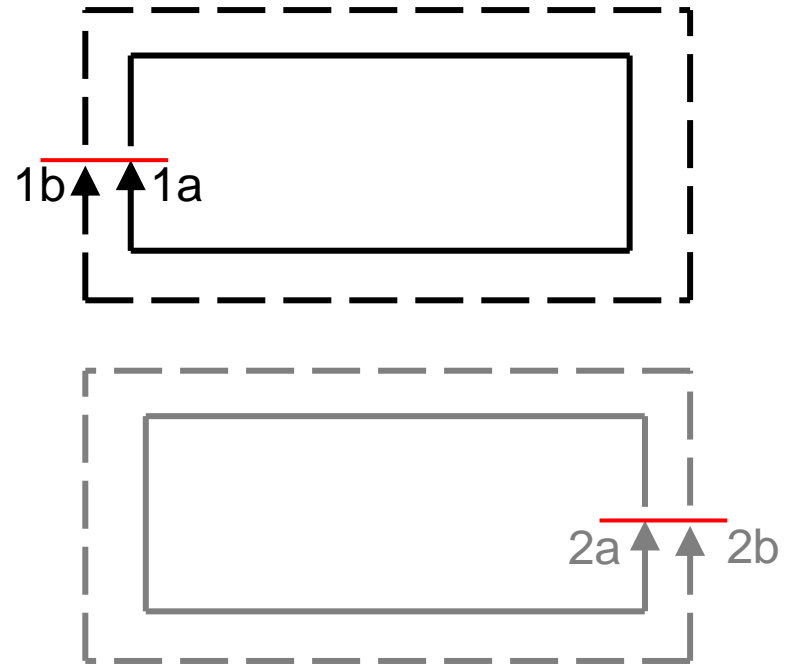
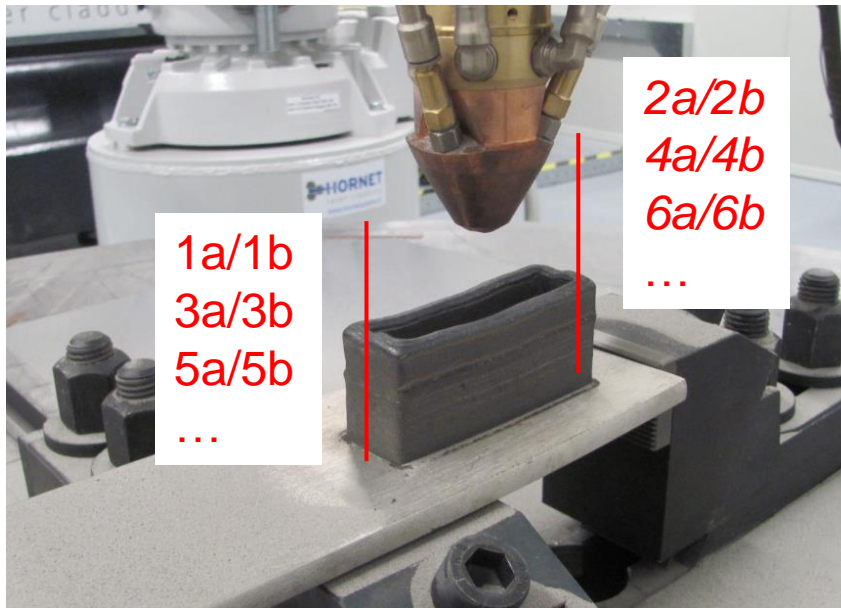
# LMD Coupon printing

# LMD Coupon printing - size

- ⌘ Deposits for mechanical characterization of 17-4PH & 316L :
  - ⌘ Walls built mainly in length vs height
  - ⌘ Wall thickness 4,5mm using 2 adjacent passes (spot size 4.5mm)
  - ⌘ Ar at 24l/min, 5min  $T_{ip}$
  - ⌘ 2500W, 1000mm/min, 30% overlap per pass
  - Walls -> hollow rectangular profiles for stable LMD deposit

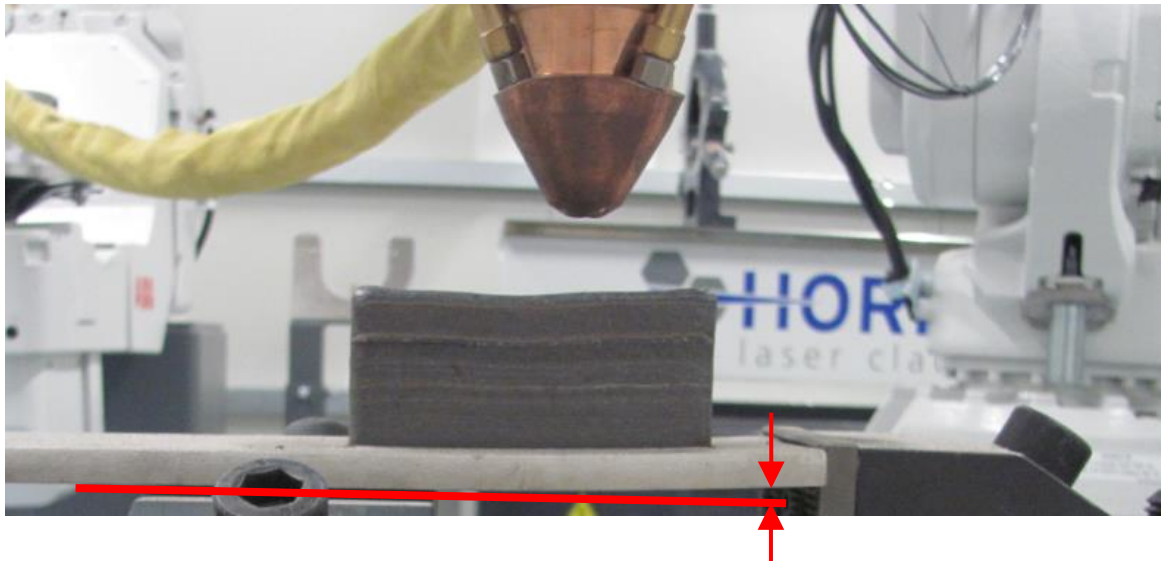


# LMD Coupon printing - strategy



- ⌘ Each 2 passes (=1 layer) switching of start/end & LMD direction
- More stable build approach (stable geometry, no overheating etc.)

# LMD Coupon printing - deformation



- ⌘ Rather important deformation of substrate
  - Substrate barely clamped
  - Less than in case of WAAM

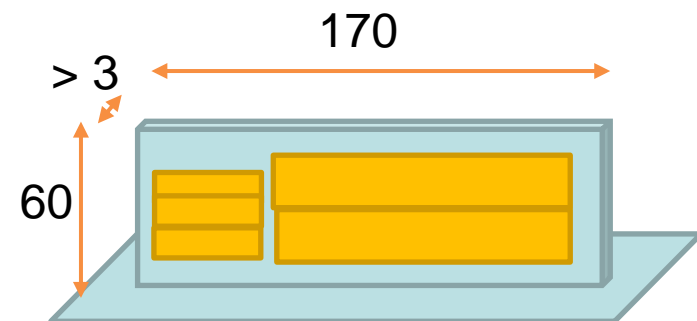
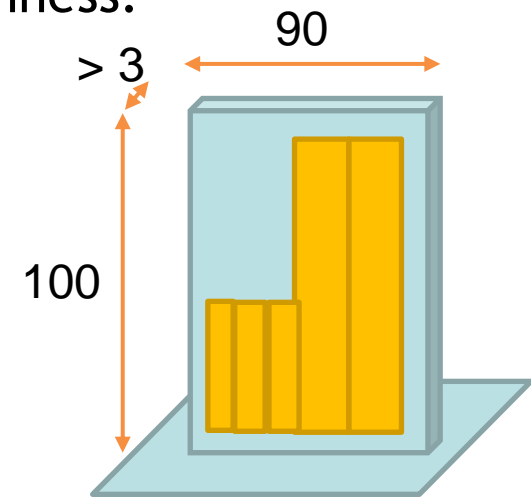
# LMD Coupon printing - Summary

- ⌘ Deposits have been performed to perform the mechanical characterization
- ⌘ An alternating strategy layer-by-layer with a closed rectangular shape is used to ensure printing stability
- ⌘ There is a noticeable deformation of the substrate

# LMD Mechanical testing

# Mechanical testing - test plan

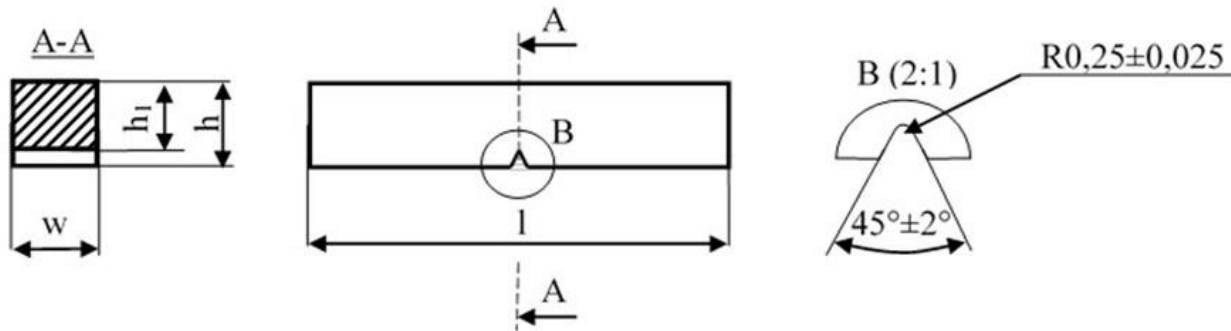
- ⌘ Hardness
- ⌘ To determine tensile strength and impact toughness:
- ⌘ Only printing of thinner walls is possible, resulting in thinner specimens:
  - ⌘ 2 flat, tensile specimen:
    - ⌘ Yield strength  $R_{eH}$  / Proof strength  $R_{p0,2}$
    - ⌘ Tensile strength  $R_m$
    - ⌘ Elongation  $A$
  - ⌘ 3 subsize-impact specimen (2,5 mm thickness)
    - ⌘ Impact toughness
- ⌘ Influence of sampling direction
  - ⌘ Multiple walls





# Mechanical testing - Impact test

- ⌘ ISO 148-1 / ISO 9016
- ⌘ Impact toughness

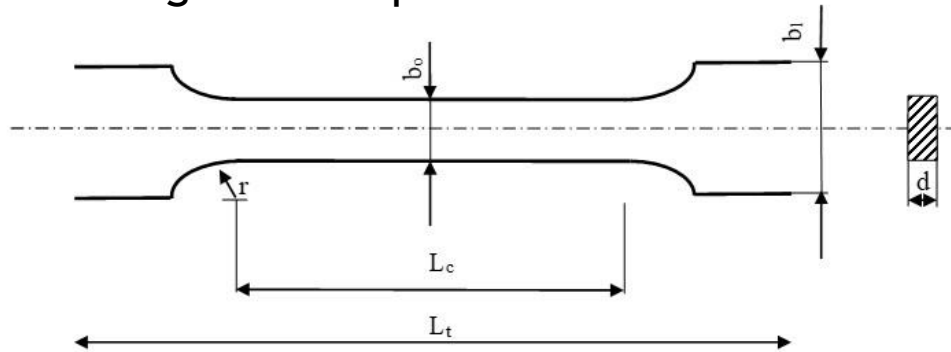


	w	h	l	h <sub>1</sub>
<input type="checkbox"/>	10 ± 0,11	10 ± 0,075	55 ± 0,60	8 ± 0,075
<input type="checkbox"/>	7,5 ± 0,11	10 ± 0,075	55 ± 0,60	8 ± 0,075
<input type="checkbox"/>	5 ± 0,06	10 ± 0,075	55 ± 0,60	8 ± 0,075
<input checked="" type="checkbox"/>	2,5 ± 0,05	10 ± 0,075	55 ± 0,60	8 ± 0,075

# Mechanical testing - Tensile test

## ⌘ ISO 6892-1

### ⌘ Tensile strength - flat specimen

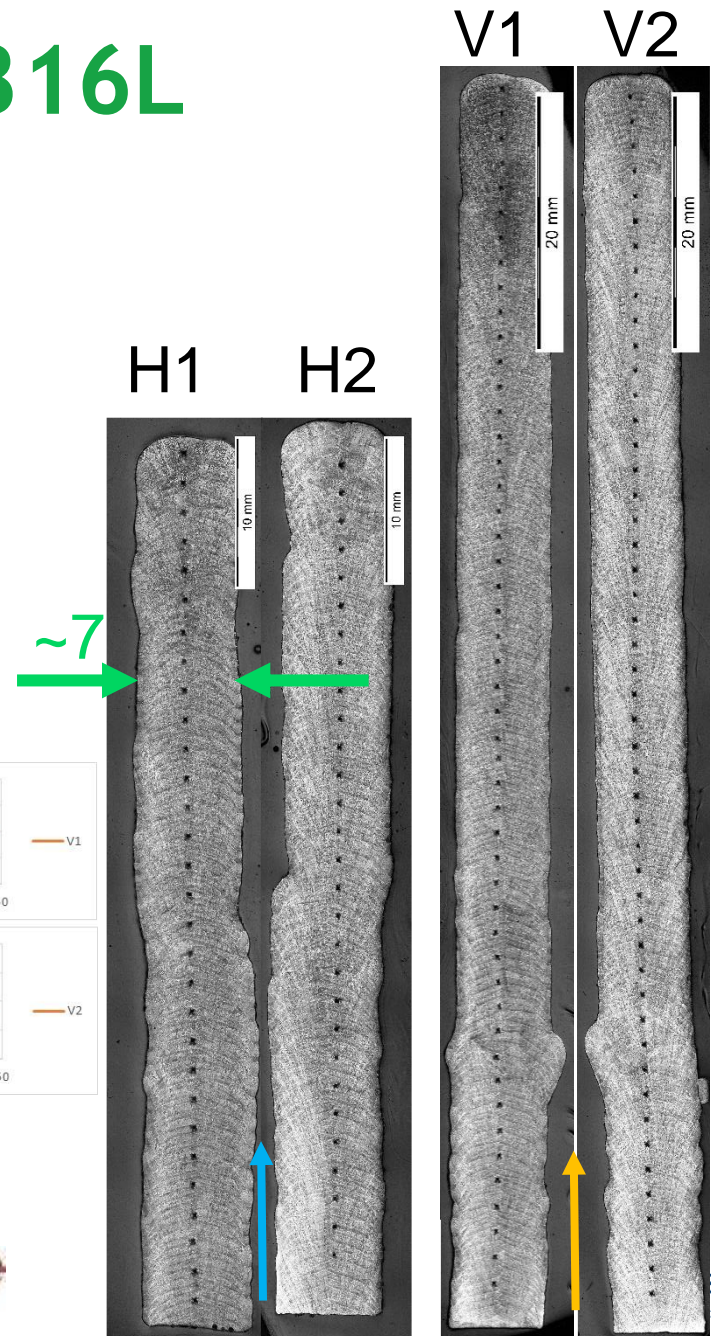
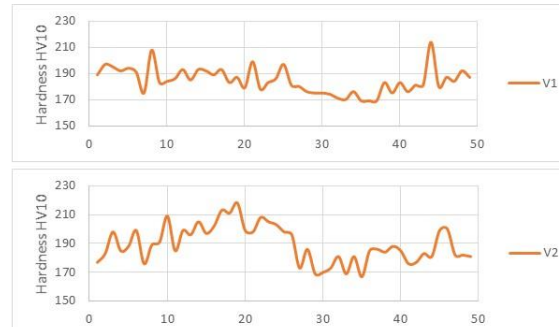
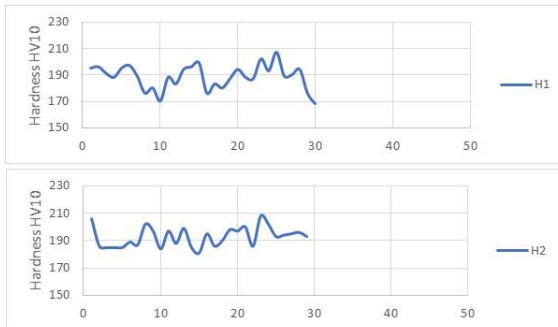


	$b_0$	$L_c$	$r$	$b_1$	$L_{t,min.}$	$d$
	<i>Proportionele proefstaven met <math>L_o = 5,65\sqrt{b_o \times d}</math>, afgerond naar de dichtsbijzijnde 5 mm</i>					
<input type="checkbox"/>	$20 \pm 0,10$		30	32		
<input type="checkbox"/>	$25 \pm 0,10$		30	37		
<input type="checkbox"/>	$40 \pm 0,15$		30	52		
<input checked="" type="checkbox"/>	$5 \pm 0,02$	26-28	12	17	90	2,5 - 3

# Mechanical testing - 316L

## Hardness

HV10	AVERAGE	MAX	MIN
H1	188	207	168
H2	193	208	181
V1	184	214	169
V2	190	218	167



# Mechanical testing - 316L

## Tensile

Longitudinal  
(X-direction)

Test specimen number	Dimension diameter d <sub>0</sub> [mm]	Test temp. T [° C]	Proof strength R <sub>p0,2</sub> [MPa]	Tensile strength R <sub>m</sub> [MPa]	Original gauge length L <sub>0</sub> [mm]	Elongation		Reduction of area Z [%]
						at R <sub>m</sub> A <sub>g</sub> [%]	after fracture A [%]	
ISL-HT11	4,030	23,1	366	590	20	-	38,0	58
ISL-HT12	4,012	23,1	345	583	20	-	28,0	58
ISL-HT21	4,023	23,1	342	547	20	-	34,0	67
ISL-HT22	4,017	23,1	387	601	20	-	39,5	57
ISL-HT31	4,020	23,1	374	590	20	-	31,0	44
ISL-HT32	4,023	23,1	364	582	20	-	25,5	44
ISL-HT41	4,009	23,1	361	590	20	-	28,0	38
ISL-HT42	4,026	23,1	356	584	20	-	34,5	58

Vertical  
(Z-direction)

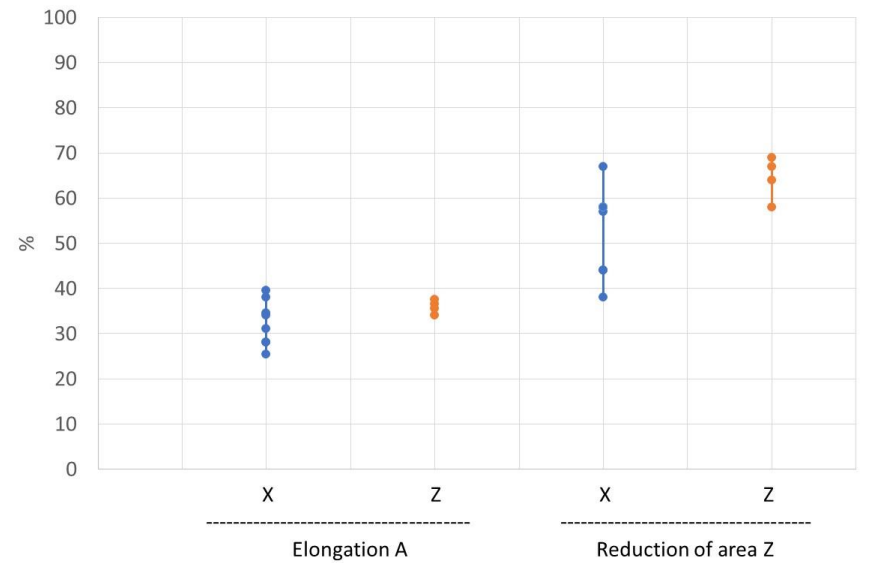
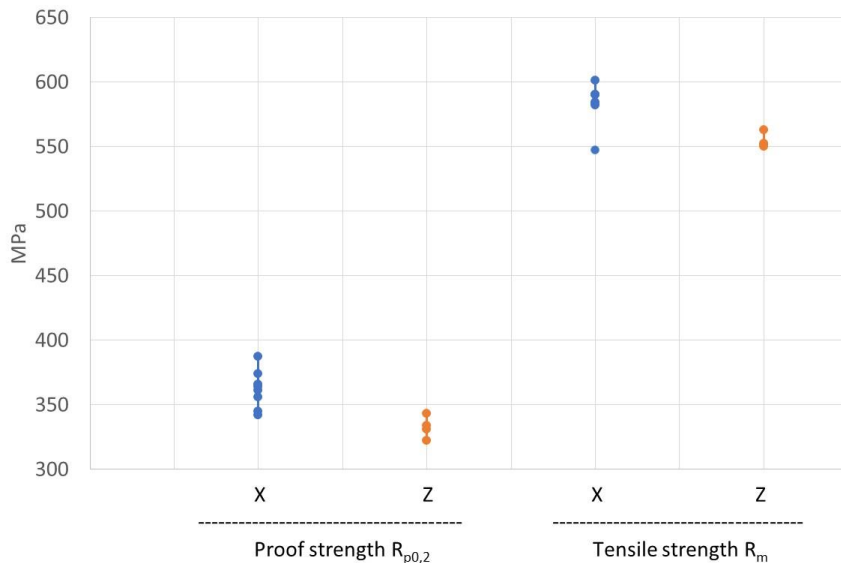
Test specimen number	Dimension diameter d <sub>0</sub> [mm]	Test temp. T [° C]	Proof strength R <sub>p0,2</sub> [MPa]	Tensile strength R <sub>m</sub> [MPa]	Original gauge length L <sub>0</sub> [mm]	Elongation		Reduction of area Z [%]
						at R <sub>m</sub> A <sub>g</sub> [%]	after fracture A [%]	
ISL-VT11	4,025	23,1	322	551	20	-	37,5	67
ISL-VT12	4,027	23,1	331	552	20	-	36,5	64
ISL-VT21	4,013	23,1	343	550	20	-	35,5	58
ISL-VT22	4,018	23,1	334	563	20	-	34,0	69

# Mechanical testing - 316L

## Tensile

- ⌘ Not substantial anisotropy between X (parallel to the base plate) & Z (perpendicular to the base plate) directions

Typical values after DED process		
316L (Höganäs)	X-direction	Z-direction
Proof strength (MPa)	355	365
Tensile strength (MPa)	508	485
Elongation A (%)	20	25

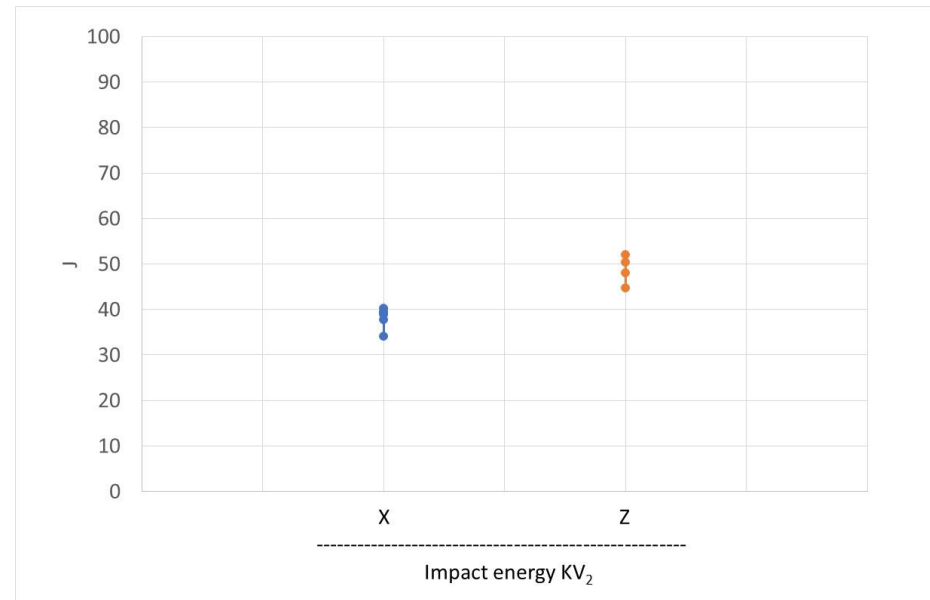
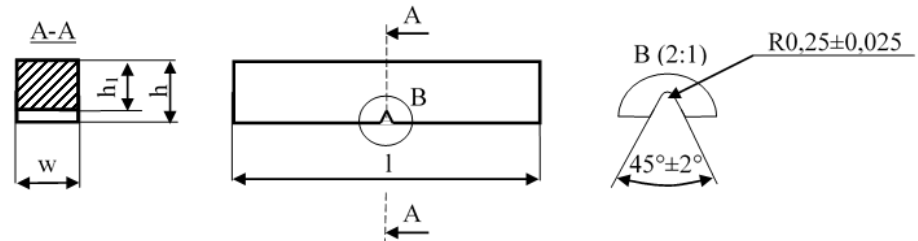


# Mechanical testing - 316L

## Impact V-notch

Specimen reference	Specimen orientation	Notch location	Size [mm]	Test temp. [° C]	Impact absorbed energy	
					KV <sub>2</sub> [J]	Average
ISL-HK1	longitudinal direction (X-direction)	through thickness	5 x 10	22	37,7	37,0
ISL-HK2					39,4	
ISL-HK3					34,0	
ISL-HK4	longitudinal direction (X-direction)	through thickness	5 x 10	22	39,3	39,4
ISL-HK5					38,8	
ISL-HK6					40,2	

Specimen reference	Specimen orientation	Notch location	Size [mm]	Test temp. [° C]	Impact absorbed energy	
					KV <sub>2</sub> [J]	Average
ISL-VK1	vertical direction (Z-direction)	through thickness	5 x 10	22	50,3	47,7
ISL-VK2					48,0	
ISL-VK3					44,7	
ISL-VK4	vertical direction (Z-direction)	through thickness	5 x 10	22	52,0	48,9
ISL-VK5					50,2	
ISL-VK6					44,4	

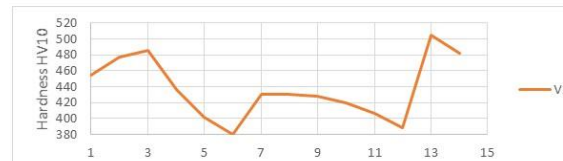
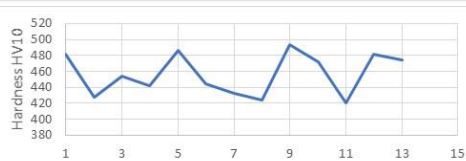
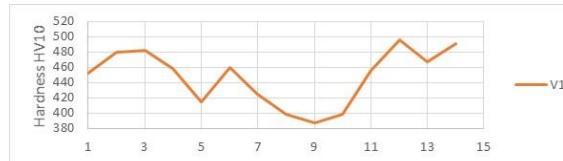
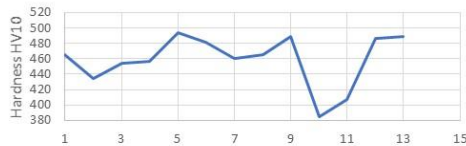
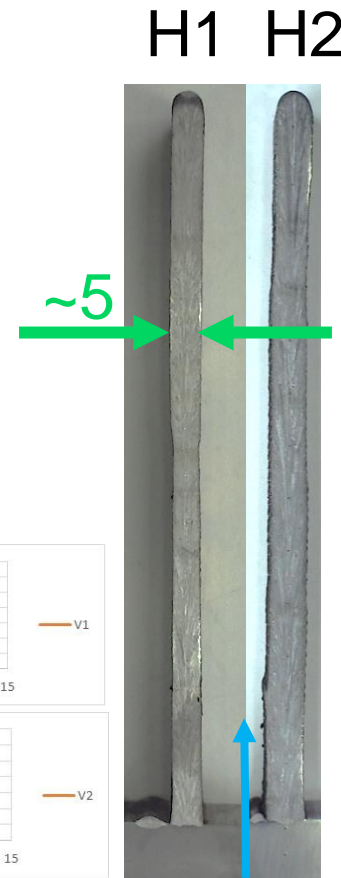


# Mechanical testing - 17-4PH

## Hardness

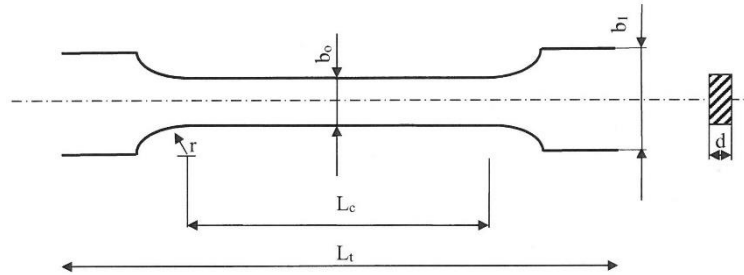
<b>Literature</b>	
<b>17-4PH-H900 (480°C-1hr)</b>	
Hardness (HV10)	375

HV10	AVERAGE	MAX	MIN
H1	459	494	385
H2	457	493	421
V1	448	496	387
V2	438	505	380



# Mechanical testing - 17-4PH

## Tensile



Test specimen number	Dimension thick. x width $a_0 \times b_0$ [mm]	Test temp. T [° C]	Yield strength $R_{eH}$ [MPa]	Proof strength $R_{p0,2}$ [MPa]	Tensile strength $R_m$ [MPa]	Original gauge length $L_0$ [mm]	Elongation		Reduction of area Z [%]
							at $R_m$ $A_g$ [%]	after fracture A [%]	
ISP-HT1	2,5 x 4,99	22	-	1104	1479	20	-	16,5	-
ISP-HT2	2,49 x 4,97	22	-	1032	1476	20	-	13,1	-
ISP-HT3	2,49 x 4,92	22	-	1102	1474	20	-	12,8	-
ISP-HT4	2,51 x 4,95	22	-	1060	1469	20	-	11,4	-
ISP-VT1	2,48 x 4,89	22	-	1029	1222	20	-	9,3	-
ISP-VT2	2,48 x 4,96	22	-	977	1221	20	-	13,4	-

Longitudinal  
(X-direction)

Vertical  
(Z-direction)

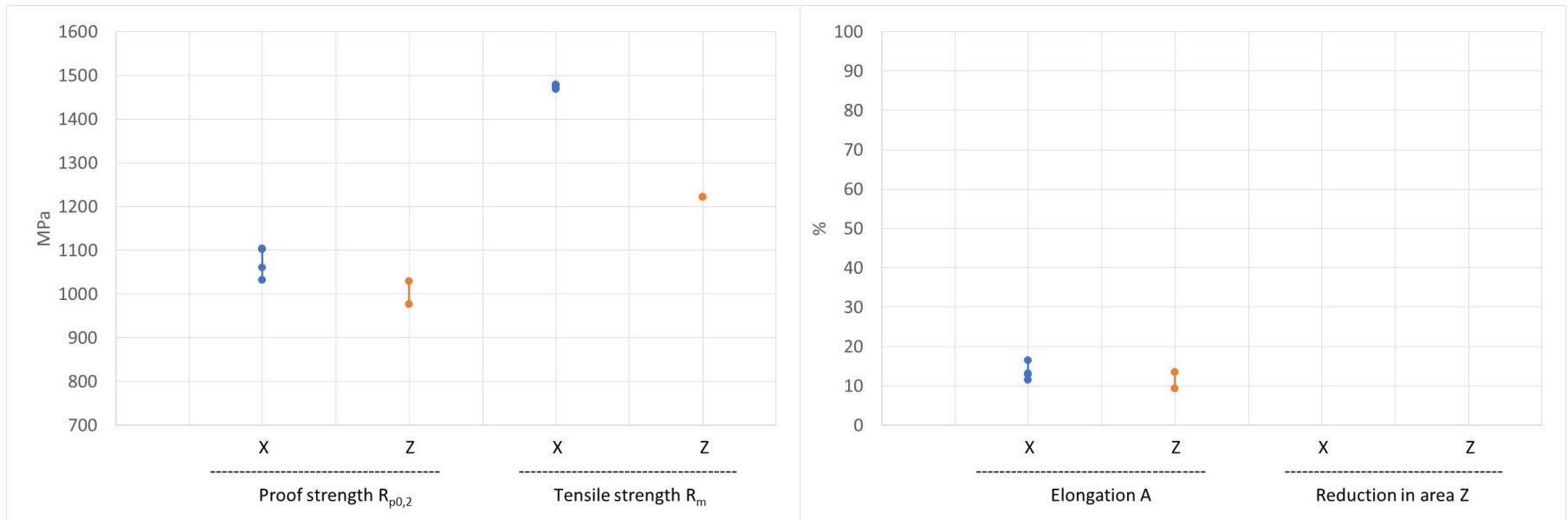


# Mechanical testing - 17-4PH

## Tensile

- ⌘ Some anisotropy between X (parallel to the base plate) & Z (perpendicular to the base plate) directions

Literature	
<b>17-4PH-H900 (480°C-1hr)</b>	
Proof strength (MPa)	945
Tensile strength (MPa)	1417
Elongation A (%)	15,5

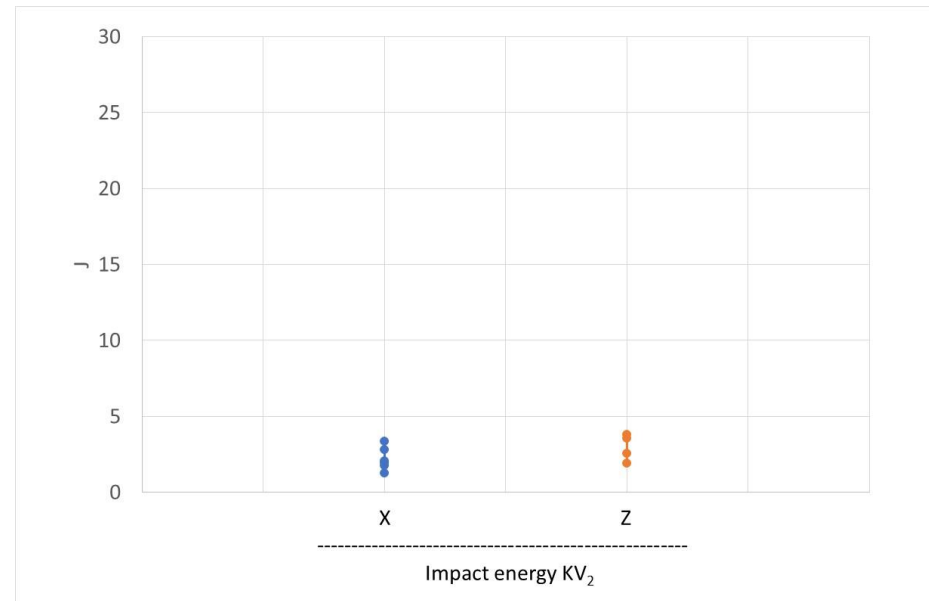
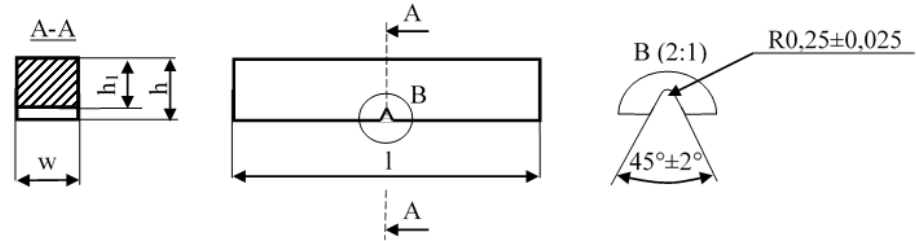


# Mechanical testing - 17-4PH

## Impact V-notch

Specimen reference	Specimen orientation	Notch location	Size [mm]	Test temp. [° C]	Impact absorbed energy	
					KV <sub>2</sub> [J]	Average
ISP-HK1	longitudinal direction (X-direction)	through thickness	2,5 x 10	22	1,7	2,1
ISP-HK2					1,3	
ISP-HK3					3,4	
ISP-HK4	longitudinal direction (X-direction)	through thickness	2,5 x 10	22	2,0	2,3
ISP-HK5					2,1	
ISP-HK6					2,8	

Specimen reference	Specimen orientation	Notch location	Size [mm]	Test temp. [° C]	Impact absorbed energy	
					KV <sub>2</sub> [J]	Average
ISP-VK1	vertical direction (Z-direction)	through thickness	2,5 x 10	22	3,8	2,7
ISP-VK2					2,5	
ISP-VK3					1,9	
ISP-VK4	vertical direction (Z-direction)	through thickness	2,5 x 10	22	3,5	3,2
ISP-VK5					3,3	
ISP-VK6					2,9	

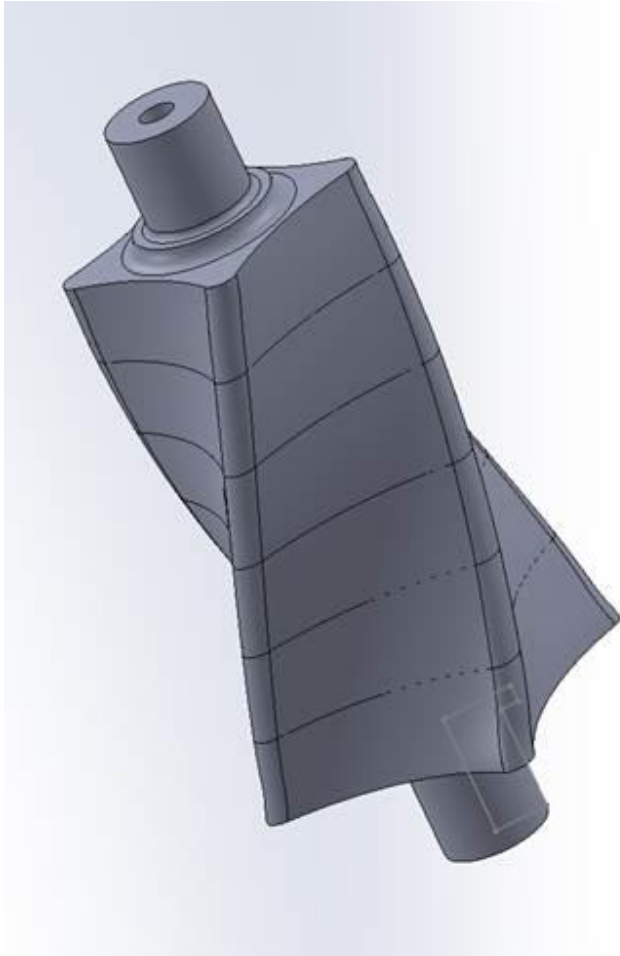


# LMD Mechanical testing- Summary

- ⌘ Some anisotropy is observed for 17-4PH but not for 316L
- ⌘ Impact results are slightly better for 316L than for 17-4PH

# Demonstrator based on LMD

# Generalized rotor



Ø Bottom: 100 mm  
Height rotor: 155 mm  
Total height: 225 mm

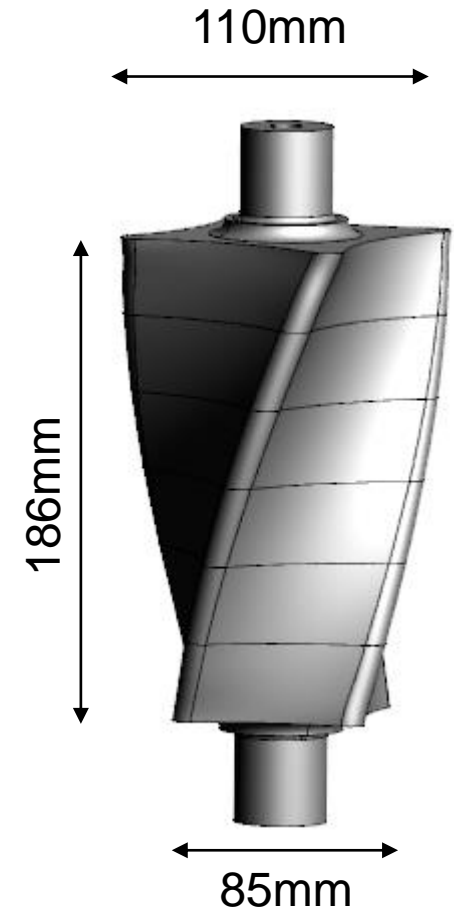
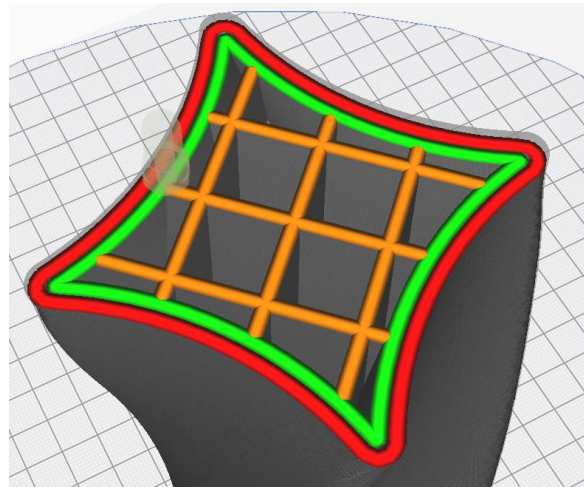
Rotation top vs. bottom: 70°  
Bevel bottom to top: 2°

Wall thickness: 3 mm

(Scale 75%)

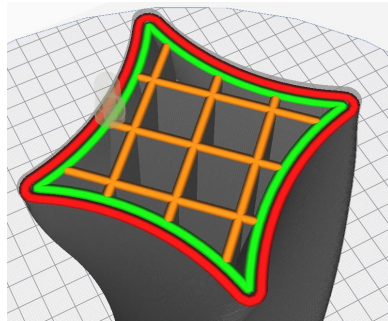
# LMD demonstrator - Pump rotor

- ⌘ Material : 17-4PH
- ⌘ Technology : laser powder (LMD)
- ⌘ Track width: 3.80 mm; Layer height: 0.47 mm
- ⌘ Printing strategy (sequence) :
  - ⌘ 2 contour lines; inner(green) & outer(red)
  - ⌘ Infill(orange)

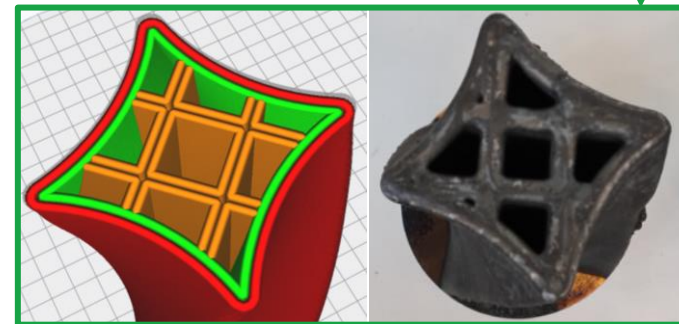
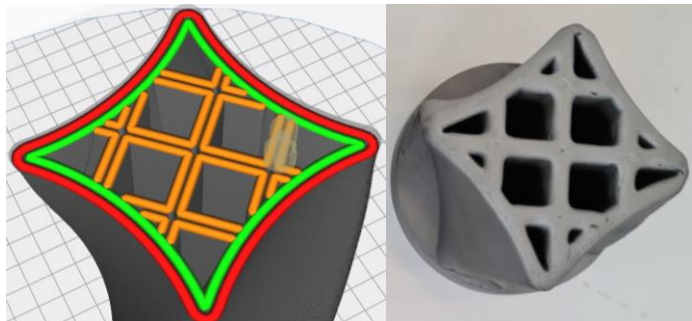


# LMD demonstrator - Pump rotor

- ⌘ 3 different infill patterns were tested :
  - ⌘ The 1<sup>st</sup> one was problematic due to crossing tracks (crossing point → overthickness!)



- ⌘ Thus 2 other patterns of different density were tested without crossing layers

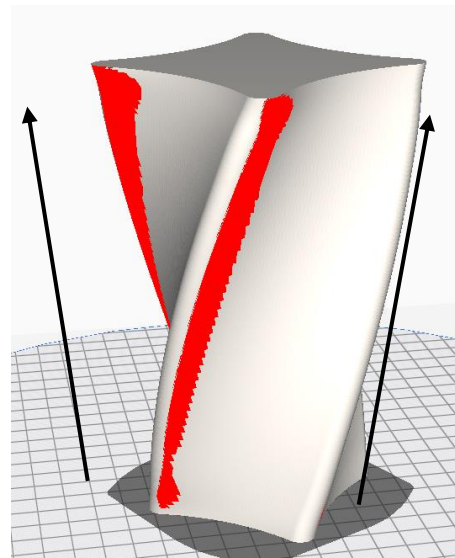


Selected filling pattern for the demonstrator

# LMD demonstrator - Pump rotor

- ⌘ The demonstrator was manufactured on machined 17-4PH axes
- ⌘ 3 trials were performed in order to reach a good result
- ⌘ 1<sup>st</sup> demonstrator failed due to the conical shape of the part → large overhanging angle (no support)

⌘ *Previous tests on hollow dome-like structures have demonstrated potential to build overhanging LMD structures up to +/- 15°*



Overhanging angle >15° in red

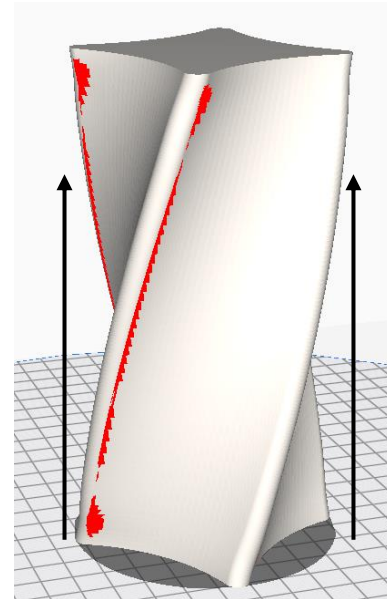


Demonstrator after sandblasting



# LMD demonstrator - Pump rotor

- ⌘ 2<sup>nd</sup> demonstrator was not conical
  - ⌘ The construction was stopped before the total height was reached → the deposition of the outer contour was problematic
  - ⌘ -> too fast
  - ⌘ At mid height, process parameters were changed and the defect was partially removed
- a 3<sup>rd</sup> demonstrator was printed with the new parameters



Overhanging angle  $>15^\circ$  in red

# LMD demonstrator - Pump rotor

- ⌘ 3<sup>rd</sup> demonstrator same as 2<sup>nd</sup> but adapted process parameters
- ⌘ The printing was successful

